## **Supplementary Information**

# Aqueous phase conversion of $\ensuremath{\text{CO}}_2$ into acetic acid over thermally

## transformed MIL-88B catalyst

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### **Characterization Results**



Fig. S1. PXRD pattern of synthesized (a) MIL-101 and Fe/MIL-101 catalyst, (b) MIL-88B, and (c) T-MIL-88B treated at different temperatures



Fig. S2: Narrow scan XPS spectra of (a) Iron 2p, (b) Chromium 2p, and (c) Carbon 1s for the studied catalysts.



Fig. S3: L<sub>2,3</sub>-edge Fe X-ray absorption near edge spectroscopy (XANES) of MIL-88B and thermally transformed MIL-88B at different temperatures



Fig. S4: (a) Thermogravimetric (TG) analysis of Fe/MIL-101 and MIL-88B under Ar atmosphere, and (b) TG and derivative thermogravimetric (DTG) analysis of MIL-88B under  $5\%H_2/N_2$  and pure  $N_2$  atmosphere.



Fig. S5: CO<sub>2</sub>-TPD analysis of T-MIL-88B-500



Fig. S6. TEM micrographs of synthesized (a) MIL-101 and (b) MIL-88B catalyst

Fable S1: Elementa	l composition o	of thermally	transformed	MIL-88B	(T-MIL-88B-5	00)
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Elements	Weight percentages (%)			
Fe*	49.3			
Na*	19.5			
C**	13.7			
H**	0.6			
N**	0.0			
S**	0.0			
O***	16.9			

\* measured by XRF analysis

\*\* measured by CHNS analysis

\*\*\* calculated on the basis of difference

#### **BET of studied catalysts**

Figure S7.a-c demonstrates the nitrogen linear isotherms of different iron based CBEA, MIL-101 and MIL-88B catalysts, respectively. The nitrogen sorption of CBEA and Fe/CBEA catalyst (Figure S7.a) represent the combination of type I and IV isotherm which interpreted that the catalyst mostly consisted with micropores <sup>1,2</sup>. The two steps nitrogen isotherm has been indicated that the presence of both micropores and mesopores in the catalyst. The micropores filling is mainly occurred in the ranges of 0<p/p°<0.05 and the mesoporous filling which leads to the appearance of hysteresis loop (H3 type) has been noticed in the ranges of 0.4<p/p°<0.9. The surface area of CBEA and reduced Fe/CBEA are 673.9 and 390.1 m<sup>2</sup>/g, respectively. The surface area of reduced Fe/CBEA is lower than the CBEA support itself which is most likely the blockage of the pore with iron. The BJH pore size distribution of CBEA support (Figure S7.d) has been revealed that the presence of mesopores in between the ranges of 1.9–50 nm. The pore diameter and the mesopore volume of this support (CBEA) is 5.3 nm and 0.11 cm<sup>3</sup>/g, respectively which has been changed minorly after the impregnation of iron as shown in Table S2. Whereas, the micropore volume of the CBEA support has changed significantly from 0.21 to 0.12 cm<sup>3</sup>/g in reduced Fe/CBEA catalyst.

The N<sub>2</sub> adsorption-desorption isotherm of MIL-101 displayed typical type I isotherm along with the secondary uptakes at p/p° ~ 0.1 and p/p° ~ 0.2 which is good agreement with the previously reported results by Fe'rey et al. <sup>3</sup>. Fe/MIL-101 also exhibits the similar type of isotherm as compared to MIL-101. After impregnation of Fe in MIL-101, the surface area of the catalyst decreased from 2473.7 cm<sup>2</sup>/g to 1831.3 cm<sup>2</sup>/g which is maybe due to the blocking of the pores with metal that is enforced by the BJH results of these two catalysts. The micropores and mesopores volume of Fe/MIL-101 are 0.09 and 0.51 cm<sup>3</sup>/g respectively which are comparatively lower than the micropore (0.35 cm<sup>3</sup>/g) and mesopore (0.60 cm<sup>3</sup>/g) volume of MIL-101

due to pore blockage. The total pore volume of Fe/MIL-101 is also lower than MIL-101 (Table S2). The degraded Fe/MIL-101 (T-Fe/MIL-101) catalyst shows (Figure S7.b) type II isotherm with H3 hysteresis loop which has a good resemblance with the results obtained for MIL-101(Cr)/RGO/ZnFe<sub>2</sub>O<sub>4</sub> nanocomposite <sup>4</sup>. The surface area of T-Fe/MIL-101 is very lower (73.5 m<sup>2</sup>/g) as compared to MIL-101 and Fe/MIL-101 which has a good resemblance with the findings obtained by Farisabadi et al. <sup>5</sup>. The poor surface area of this aforementioned catalyst is most likely due to the collapse of organic framework which was previously articulated by Li et al. for MIL-101-Cr MOF that was thermally treated at 550 °C <sup>6</sup>. In the low-pressure region, the absence of adsorption suggested that all micropores in MIL-101 are collapsed and the existence of hysteresis loop in the high-pressure region indicated the presence of mesopores <sup>6</sup>.

Figure S7.c represented N<sub>2</sub> adsorption-desorption isotherm of MIL-88B and T-MIL-88B-500. MIL-88B exhibits the type I isotherm that suggesting the microporous MOF with high surface area (410.6 m<sup>2</sup>/g) which is almost similar with the results reported by Vu et al. <sup>7</sup>. The pore size distribution of MIL-88B is displayed in Figure S7.f and the average pore diameter is 6.1 nm with total pore volume (both micropore and mesopore) of 0.32 cm<sup>3</sup>/g. The N<sub>2</sub> adsorption-desorption isotherm of T-MIL-88B-500 is type II with H2 (b)-type hysteresis loop which is identical with the results obtained for MIL-88B that was thermally degraded at 500 °C under N<sub>2</sub> atmosphere <sup>8</sup>. Due to the presence of mesopores, the high-pressure region of the isotherm consisted with hysteresis loop. Table S2 showed that the surface area of T-MIL-88B-500 catalyst is lower (160.6 m<sup>2</sup>/g) than MIL-88B which is most likely due to collapse of organic matrix <sup>9</sup>.





Fig. S7. Nitrogen sorption isotherms of (a) CBEA, (b) MIL-101, and (c) MIL-88B based Fe catalysts, respectively; and BJH desorption pore distribution of (d) CBEA, (e) MIL-101, and (f) MIL-88B based Fe catalysts, respectively.

Nanomaterials	<sup>†</sup> Sbet	$^{\dagger\dagger}D_{Pore}$	⁺V <sub>micro</sub>	<sup>⊦⊦</sup> V <sub>meso</sub>	HH-Vtotal
	(m²/g)	(nm)	(cm <sup>3</sup> /g)	(cm <sup>3</sup> /g)	(cm <sup>3</sup> /g)
CBEA	673.9	5.3	0.21	0.11	0.32
Reduced 10%Fe/CBEA	390.1	6.4	0.12	0.13	0.25
MIL-101	2473.7	3.0	0.35	0.60	0.95
10%Fe/MIL-101	1831.3	2.8	0.09	0.51	0.60
T-10%Fe/MIL-101	73.5	20.2	0.00	0.38	0.38
MIL-88B	410.6	6.1	0.09	0.23	0.32
T-MIL-88B-500	160.6	14.2	0.04	0.27	0.31

Table S2: Physical and textural characteristics of studied supports and catalysts

<sup>†</sup> surface area via Brunauer-Emmett-Teller (BET) method

<sup>††</sup> Mean desorption diameter of pore via Barrett-Joyner-Halenda (BJH) method

<sup>+</sup> Cumulative desorption pore volume via Barrett-Joyner-Halenda (BJH) method

<sup>++</sup> Micropore volume via t-plot

**HH** Total volume of pores

#### GC chromatograms for gaseous products



Fig. S8. GC chromatograms of (a) FID and (b) TCD detectors for gas sample of aqueous phase CO<sub>2</sub> hydrogenation using T-MIL-88B-500 in the presence of CH<sub>3</sub>OH and LiI. Reaction conditions: T= 150 °C,  $H_2/CO_2= 1$ ,  $t_R= 48h$ ,  $P_{total}= 70$  bar at room temperature and stirring speed= 200 RPM. GC chromatograms of (c) FID and (d) TCD detectors for gas sample of standard calibration gas mixture. Composition of standard calibration gas mixture: 20.20% CO, 20.43% H<sub>2</sub>, 10.08% CH<sub>4</sub>, 10.09% CO<sub>2</sub> and 39.2% N<sub>2</sub>.



Fig. S9. Standard calibration curves of (a) acetic acid and (b) formic acid in Milli-Q water

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